

# The optimization of control parameters $K_v$ and $K_p$

Based on Computed Torque

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# Computed Torque

We are given a description of the dynamics of a robot manipulator in the form of the equation

$$M(\theta)\ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + G(\theta, \dot{\theta}) = \tau \quad (1)$$

Consider the following control law:

$$\tau = M(\theta)(\ddot{\theta}_d - K_v \dot{e} - K_p e) + C(\theta, \dot{\theta})\dot{\theta} + N(\theta, \dot{\theta}) \quad (2)$$

Where  $e = \theta - \theta_d$  and  $K_v$  and  $K_p$  are constant gain matrices

When substituted into equation (1), the error dynamics can be written as:

$$M(\theta)(\ddot{e} + K_v \dot{e} + K_p e) = 0$$

Since  $M(\theta)$  is always positive definite, we have

$$\ddot{e} + K_v \dot{e} + K_p e = 0$$

To be continued

Consider the following differential equation group:

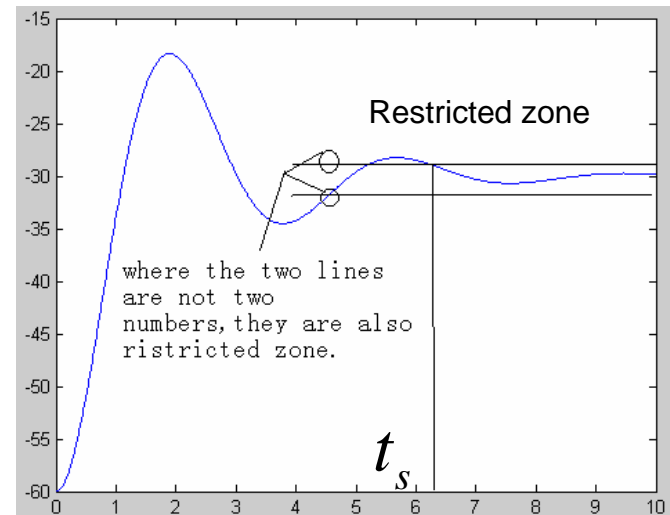
$$\ddot{e} + K_v \dot{e} + K_p e = 0$$

If we can solve the vector  $e$ , then we can get the settle time of system  $t_s$

Analytic Solution and Numerical solution :

1. Analytic Solution: using matlab function “dsolve()”
2. Numerical Solution: Using ODE45 integration method

Given a restricted zone , then search the value like  $t_s$



## Analytic Solution based on diag

$$k_p = \omega_n^2$$

$$kv = 2\xi\omega_n$$

$$\Delta = 0.05$$

$$t_s = \frac{3 + \ln \frac{1}{\sqrt{1 - \xi^2}}}{\xi\omega_n} = \frac{3 + \ln \frac{1}{\sqrt{1 - \frac{kv^2}{4kp}}}}{0.5kv}$$

brought forward, continued

$$\ddot{e} + K_v \dot{e} + K_p e = 0$$

So consider the step response

$$\begin{pmatrix} \ddot{e}_1 \\ e_1 \\ \ddot{e}_2 \\ e_2 \\ \ddot{e}_3 \\ e_3 \end{pmatrix} + \begin{pmatrix} k_{v11} & k_{v12} & k_{v13} \\ k_{v21} & k_{v22} & k_{v23} \\ k_{v31} & k_{v32} & k_{v33} \end{pmatrix} \begin{pmatrix} \dot{e}_1 \\ e_1 \\ \dot{e}_2 \\ e_2 \\ \dot{e}_3 \\ e_3 \end{pmatrix} + \begin{pmatrix} k_{p11} & k_{p12} & k_{p13} \\ k_{p21} & k_{p22} & k_{p23} \\ k_{p31} & k_{p32} & k_{p33} \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = 0$$

That the  $K_v$  and  $K_p$  are constant gain matrices, both of them are 3-by-3 matrices.

## Discussion on $K_v$ and $K_p$

Since our equation is linear, it is easy to choose  $K_v$  and  $K_p$  so that the overall system is stable and  $e \rightarrow 0$  exponentially as  $t \rightarrow \infty$ . Moreover, we can choose  $K_v$  and  $K_p$  such that we get independent exponentially stable systems (by choosing  $K_v$  and  $K_p$  diagonal)

At first, to simplify the optimization procedure, consider  $K_v$  and  $K_p$  as diagonal matrix:

$$K_v = \begin{pmatrix} k_{v11} & 0 & 0 \\ 0 & k_{v22} & 0 \\ 0 & 0 & k_{v33} \end{pmatrix} \quad K_p = \begin{pmatrix} k_{p11} & 0 & 0 \\ 0 & k_{p22} & 0 \\ 0 & 0 & k_{p33} \end{pmatrix}$$

For the three arms are coupling, that the general condition is following form:

$$K_v = \begin{pmatrix} k_{v11} & k_{v12} & k_{v13} \\ k_{v21} & k_{v22} & k_{v23} \\ k_{v31} & k_{v32} & k_{v33} \end{pmatrix} \quad K_p = \begin{pmatrix} k_{p11} & k_{p12} & k_{p13} \\ k_{p21} & k_{p22} & k_{p23} \\ k_{p31} & k_{p32} & k_{p33} \end{pmatrix}$$

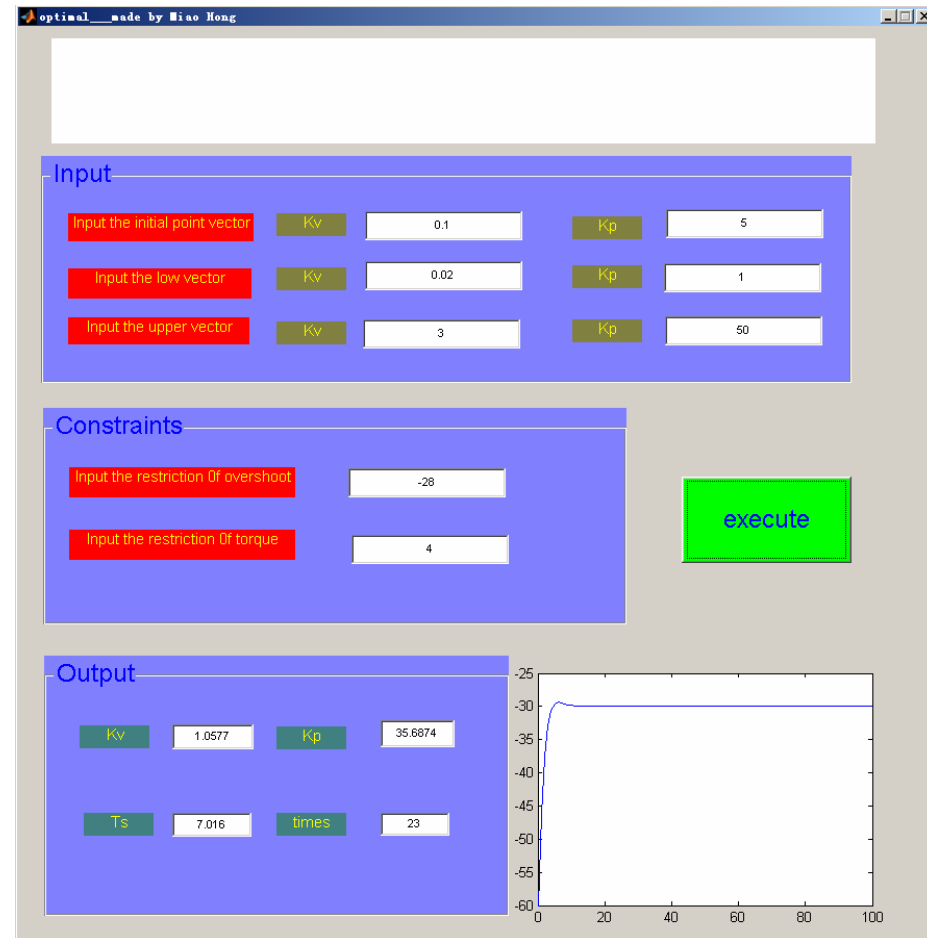
# Attempt 1

Using a random algorithm (CRS) and  $K_v$   $K_p$  are diagonal matrix

Minimize the settle time  $t_s$

Given the constraint condition: Overshoot and Torque

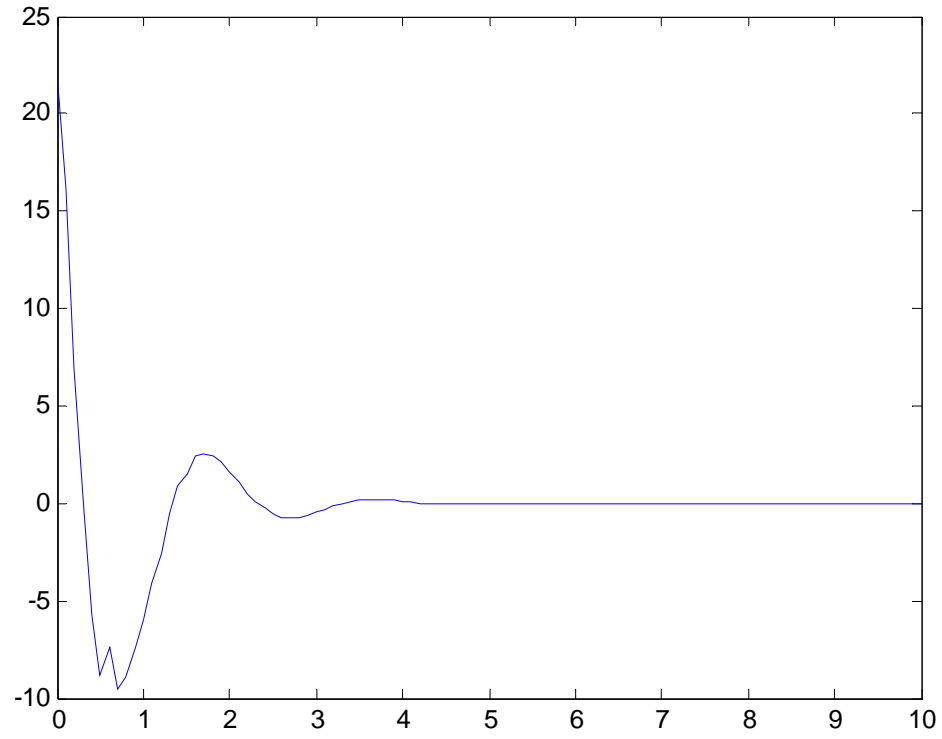
Using CRS algorithm (a random algorithm)

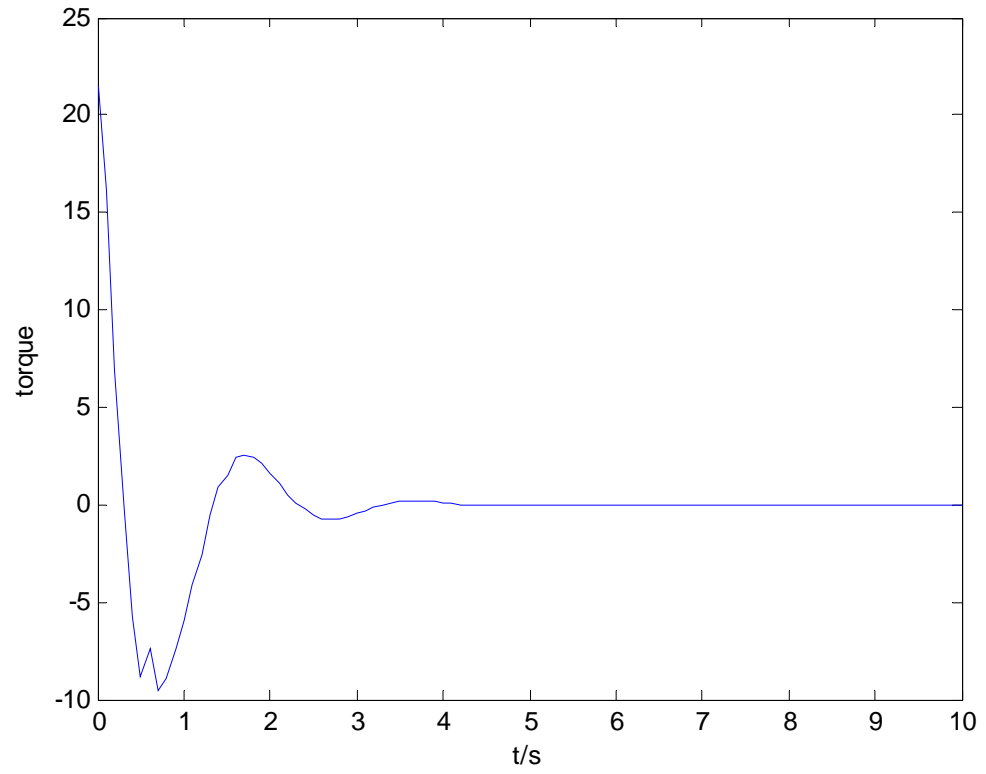


Ts:5%, torque=8

<b>I tem</b> serial number	$K_v$	$K_p$	$t_s$	zone
<b>1</b>	<b>2.5422</b>	<b>27.6986</b>	<b>2.6270</b>	(0.01 10) (1 30)
<b>2</b>	<b>2.7137</b>	<b>27.6232</b>	<b>2.5800</b>	(0.01 20) (10 40)
<b>3</b>	<b>2.8040</b>	<b>40.2054</b>	<b>2.2080</b>	(0.1 30) (10 100)
<b>4</b>	<b>3.1482</b>	<b>49.0453</b>	<b>1.9950</b>	(1 20) (30 100)
<b>5</b>	<b>3.9381</b>	<b>83.5124</b>	<b>1.5360</b>	(1 40) (50 200)







## Attempt 2

$K_v$   $K_p$  are full matrix

Using DE (Differential Evolution ) algorithm

Given the constraint condition: Overshoot and Torque

	$K_v$ $K_p$	$t_s$
1	[4.26706597 14.92405344 4.05558081 11.07597856 1.37044929 10.98976583 10.81332597 9.77559251 7.14290767 8.34374800 2.16020216 19.02660746 3.76842172 4.84391167 3.75787337 1.82821512 9.89138987 6.65297016]	26.70000000
2	[8.38415344 9.66491588 2.82934740 8.48853407 4.03860291 0.46114840 8.46650245 29.30018339 9.91270916 9.75393670 6.20485862 14.71557669 4.86861018 8.46452498 1.19715496 2.47733172 9.85699738 9.88032570]	1.90000000
3	[1.72673409 1.44809618 1.19204083 1.71647225 1.91543135 1.20000000 1.63146158 1.10856461 1.12551764 1.59470321 1.28321770 1.26734351 2.52512542 1.55333279 1.09185410 1.51563279 1.20000000 1.86734762]	1.40000000
4	[11.06984902 18.72165141 1.62312409 9.31282423 12.64859416 6.83273190 6.71091474 5.91628608 7.81480318 2.74264273 9.97740450 1.92199301 3.13046826 17.45543587 3.20369254 15.61417119 4.85298320 14.62482400]	0.40000000
5	[20.65988912 17.19640978 4.69860201 11.84740403 22.05042745 8.26414227 16.63362331 5.15625052 0.66985597 5.75128478 2.16823081 2.56862454 15.20386660 20.63099331 7.46930910 6.66251992 9.85351572 27.14483642]	0.30000000

## Research on the distinction between the full matrix and diagonal matrix

If we choosing  $K_v$  and  $K_p$  as diagonal, that we can get independent system (three independent systems ).

But the three arms are coupling, so the general situation is that  $K_v$  and  $K_p$  are not diagonal matrix.

To be continued

Consider a damped free oscillation, The dynamics of the system are given by the following equation

$$M \ddot{q} + B \dot{q} + Kq = 0$$

Where M,B, and K are all positive quantities. As a state space equation we rewrite equation as

$$\frac{d}{dt} \begin{bmatrix} q \\ \dot{q} \end{bmatrix} = \begin{bmatrix} \dot{q} \\ -(K/M)q - (B/M)\dot{q} \end{bmatrix}$$

Since this system is a linear system, we can determine stability by examining the poles of the system. The Jacobian matrix for the system is

$$A = \begin{pmatrix} 0 & 1 \\ -K/M & -B/M \end{pmatrix}$$

Which has a characteristic equation

$$\lambda^2 + (B/M)\lambda + (K/M) = 0$$

To be continued

The solutions of the characteristic equation are

$$\lambda = \frac{-B \pm \sqrt{B^2 - 4KM}}{2M}$$

Which always have negative real parts, and hence the system is globally exponentially stable.

From the pp248 (A Mathematical Introduction to Robotic Manipulation<sup>[1]</sup>), we know the stability is established on diagonal matrix .

So we can see that if we restrict the matrix to diagonal , we may lose a lot of stability based on full matrix .

As we've seen , the full matrix is more general , it covered every stability , so it is more reasonable. Conversely , the diagonal matrix will lose a lot of reasonable results.

So we can predict that the result of full matrix is better than diagonal .

$$A = \begin{pmatrix} 0 & M \\ -M^{-1} * Kp & -M^{-1} * Kv \end{pmatrix}$$

$$M = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$Kp = \begin{pmatrix} k_{p11} & k_{p12} & k_{p13} \\ k_{p21} & k_{p22} & k_{p23} \\ k_{p31} & k_{p32} & k_{p33} \end{pmatrix}$$

$$Kv = \begin{pmatrix} k_{v11} & k_{v12} & k_{v13} \\ k_{v21} & k_{v22} & k_{v23} \\ k_{v31} & k_{v32} & k_{v33} \end{pmatrix}$$

$$A = \begin{pmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ -Kp11 & -Kp12 & -Kp13 & -Kv11 & -Kv12 & -Kv13 \\ -Kp21 & -Kp22 & -Kp23 & -Kv21 & -Kv22 & -Kv23 \\ -Kp31 & -Kp32 & -Kp33 & -Kv31 & -Kv32 & -Kv33 \end{pmatrix};$$

Eigenvalues [A]



We get the characteristic equation of A:

$$\begin{aligned} & \_Z^6+(kv33+kv22+kv11)\_Z^5+(-kv23*kv32+kp11+kp22- \\ & kv21*kv12+kv11*kv22+kp33+kv11*kv33+kv22*kv33- \\ & kv31*kv13)\_Z^4+(kp11*kv22-kv11*kv23*kv32-kv13*kp31-kv21*kp12- \\ & kv31*kv13*kv22-kv12*kp21+kv21*kv13*kv32+kv11*kp33- \\ & kv31*kp13+kp11*kv33+kv11*kv22*kv33- \\ & kv21*kv12*kv33+kv11*kp22+kp22*kv33+kv31*kv12*kv23+kv22*kp33-kp23*kv32- \\ & kv23*kp32)\_Z^3+(-kp11*kv23*kv32-kv11*kp23*kv32-kv21*kv12*kp33- \\ & kp13*kp31+kv21*kv13*kp32+kv21*kp13*kv32+kp22*kp11+kv23*kv12*kp31+kv3 \\ & 1*kv12*kp23+kv31*kp12*kv23-kv22*kv13*kp31+kp22*kp33-kv31*kv13*kp22- \\ & kv31*kp13*kv22-kv12*kp21*kv33-kp12*kp21- \\ & kv21*kp12*kv33+kv13*kp21*kv32+kv11*kv22*kp33+kp33*kp11-kp23*kp32- \\ & kv11*kv23*kp32+kv11*kp22*kv33+kp11*kv22*kv33)\_Z^2+(-kv22*kp13*kp31- \\ & kv12*kp21*kp33-kp11*kv23*kp32- \\ & kv21*kp12*kp33+kv13*kp21*kp32+kv23*kp12*kp31+kp23*kv12*kp31+kv21*kp13 \\ & *kp32+kp11*kp22*kv33-kp22*kv13*kp31+kp13*kp21*kv32+kv31*kp12*kp23- \\ & kp11*kp23*kv32-kp12*kp21*kv33-kv11*kp23*kp32- \\ & kv31*kp13*kp22+kp11*kv22*kp33+kv11*kp22*kp33)\_Z+kp23*kp12*kp31+kp11* \\ & kp22*kp33-kp22*kp13*kp31+kp13*kp21*kp32-kp11*kp23*kp32- \\ & kp12*kp21*kp33=0 \end{aligned}$$

So we write this equation as:

$$Z^6 + a_1 Z^5 + a_2 Z^4 + a_3 Z^3 + a_4 Z^2 + a_5 Z + a_6 = 0$$

Where

$$a_1 = kv33+kv22+kv11$$

$$a_2 = -kv23*kv32+kp11+kp22-kv21*kv12+kv11*kv22+kp33+kv11*kv33+kv22*kv33-kv31*kv13$$

$$a_3 = kp11*kv22-kv11*kv23*kv32-kv13*kp31-kv21*kp12-kv31*kv13*kv22-kv12*kp21+kv21*kv13*kv32+kv11*kp33-kv31*kp13+kv11*kv33+kv11*kv22*kv33-kv21*kv12*kv33+kv11*kp22+kp22*kv33+kv31*kv12*kv23+kv22*kp33-kp23*kv32-kv23*kp32$$

$$a_4 = -kp11*kv23*kv32-kv11*kp23*kv32-kv21*kv12*kp33-kp13*kp31+kv21*kv13*kp32+kv21*kp13*kv32+kp22*kp11+kv23*kv12*kp31+kv31*kv12*kp23+kv31*kp12*kv23-kv22*kv13*kp31+kp22*kp33-kv31*kv13*kp22-kv31*kp13*kv22-kv12*kp21*kv33-kp12*kp21-kv21*kp12*kv33+kv13*kp21*kv32+kv11*kv22*kp33+kp33*kp11-kp23*kp32-kv11*kv23*kp32+kv11*kp22*kv33+kp11*kv22*kv33$$

$$a_5 = -kv22*kp13*kp31-kv12*kp21*kp33-kp11*kv23*kp32-kv21*kp12*kp33+kv13*kp21*kp32+kv23*kp12*kp31+kp23*kv12*kp31+kv21*kp13*kp32+kp11*kp22*kv33-kp22*kv13*kp31+kp13*kp21*kv32+kv31*kp12*kp23-kp11*kp23*kv32-kp12*kp21*kv33-kv11*kp23*kp32-kv31*kp13*kp22+kp11*kv22*kp33+kv11*kp22*kp33$$

$$a_6 = kp23*kp12*kp31+kp11*kp22*kp33-kp22*kp13*kp31+kp13*kp21*kp32-kp11*kp23*kp32-kp12*kp21*kp33$$

To determine the stability of a polynomial , one can simply compute the roots of the polynomial.

So using Routh Criterion, then  $a_i > 0, i=1, \dots, n$

We can get the requirement of stability.

$$A = \begin{pmatrix} 0 & M \\ -M^{-1} * Kp & -M^{-1} * Kv \end{pmatrix}$$

$$M = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$Kp = \begin{pmatrix} k_{p11} & k_{p12} & k_{p13} \\ k_{p21} & k_{p22} & k_{p23} \\ k_{p31} & k_{p32} & k_{p33} \end{pmatrix}$$

$$Kv = \begin{pmatrix} k_{v11} & k_{v12} & k_{v13} \\ k_{v21} & k_{v22} & k_{v23} \\ k_{v31} & k_{v32} & k_{v33} \end{pmatrix}$$

Mx=[1 0 0;0 1 0;0 0 1];

Kx=[k11 k12 k13;k21 k22 k23;k31 k32  
k33];

Cx=[c11 c12 c13;c21 c22 c23;c31 c32  
c33];

part1=[0 0 0;0 0 0;0 0 0];

part2=[1 0 0;0 1 0;0 0 1];

part3=-inv(Mx)\*Kx;

part4=-inv(Mx)\*Cx;

whole=[part1 part2;part3 part4];

value=eig(whole);  
valuex=real(value);  
valuex

valuex = -16.5378 5.8292 5.8292 -2.9461 -0.3716 -0.7789  
valuex = -28.3576 -5.9326 -5.9326 2.8237 -0.7346 0.9206  
valuex = -28.2471 -2.9038 -2.9038 -0.3336 -0.3336 1.0525  
valuex = -34.5607 17.1064 -8.1646 0.7414 -0.1984 -1.3434  
valuex = -24.8227 -9.7191 -0.9422 -0.9422 -0.2106 -0.2106  
valuex = -28.7259 6.0426 -7.2991 0.4536 -1.3840 -0.4590  
valuex = -28.1506 1.1907 1.1907 -0.0246 -1.7298 -1.7298  
valuex = -41.2884 -16.0734 -5.7253 -0.2879 -0.2879 0.1309  
valuex = -31.8587 -14.4796 4.6232 1.7373 0.0134 -0.4491  
valuex = -34.6612 9.6515 -11.0541 0.1651 -0.5390 -1.3423  
valuex = -35.3750 -13.7301 3.8697 -1.9434 0.1045 -0.6924

	Best solution(Diag)	Best solution(Full)	$t_s$ (diag)	$t_s$ (full)
1	2.3833 3.3421	[8.38415344 9.66491588 2.82934740 8.48853407 4.03860291 0.46114840 8.46650245 29.30018339 9.91270916 9.75393670 6.20485862 14.71557669 4.86861018 8.46452498 1.19715496 2.47733172  9.85699738 9.88032570]	3.7500	1.90000000
2	1.5217 1.9587	[1.72673409 1.44809618 1.19204083 1.71647225 1.91543135 1.20000000 1.63146158 1.10856461 1.12551764 1.59470321 1.28321770 1.26734351 2.52512542 1.55333279 1.09185410 1.51563279 1.20000000 1.86734762]	4.4310	1.40000000
3	1.3129 1.0761	[20.65988912 17.19640978 4.69860201 11.84740403 22.05042745 8.26414227 16.63362331 5.15625052 0.66985597 5.75128478 2.16823081 2.56862454 15.20386660 20.63099331 7.46930910 6.66251992  9.85351572 27.14483642]	6.4900	0.30000000
4	1.1431 1.0448	[11.06984902 18.72165141 1.62312409 9.31282423 12.64859416 6.83273190 6.71091474 5.91628608 7.81480318 2.74264273 9.97740450 1.92199301 3.13046826 17.45543587 3.20369254 15.61417119  4.85298320 14.62482400]	6.1510	0.40000000

**Thank you!!**